



FAN5361 6MHz, 600mA Synchronous Buck Regulator

Features

- 6MHz Fixed-Frequency Operation
- 35µA Typical Quiescent Current
- Best-in-Class Load Transient Response
- Best-in-Class Efficiency
- 600mA Output Current Capability
- 2.3V to 5.5V Input Voltage Range
- 1.0 to 1.82V Fixed Output Voltage
- Low Ripple Light-Load PFM Mode
- Forced PWM and External Clock Synchronization
- Internal Soft-Start
- Input Under-Voltage Lockout (UVLO)
- Thermal Shutdown and Overload Protection
- 6-bump WLCSP, 0.4mm Pitch

Applications

- Cell Phones, Smart Phones
- 3G, WiFi[®], WiMAX[™], and WiBro[®] Data Cards
- Netbooks[®], Ultra-Mobile PCs

Description

The FAN5361 is a 600mA, step-down, switching voltage regulator that delivers a fixed output from an input voltage supply of 2.3V to 5.5V. Using a proprietary architecture with synchronous rectification, the FAN5361 is capable of delivering a peak efficiency of 92%, while maintaining efficiency over 80% at load currents as low as 1mA.

The regulator operates at a nominal fixed frequency of 6MHz, which reduces the value of the external components to 470nH for the output inductor and 4.7μ F for the output capacitor. The PWM modulator can be synchronized to an external frequency source.

At moderate and light loads, pulse frequency modulation is used to operate the device in power-save mode with a typical quiescent current of 35 μA . Even with such a low quiescent current, the part exhibits excellent transient response during large load swings. At higher loads, the system automatically switches to fixed-frequency control, operating at 6MHz. In shutdown mode, the supply current drops below $1\mu A$, reducing power consumption. For applications that require minimum ripple or fixed frequency, PFM mode can be disabled using the MODE pin.

The FAN5361 is available in 6-bump, 0.4mm pitch, Wafer-Level Chip-Scale Package (WLCSP).

Typical Application

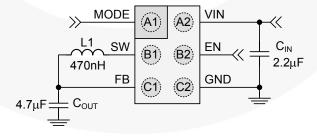


Figure 1. Typical Application

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WiMax™ is a trademark of WIMAX Forum Corporation.

WiBro® is a registered trademark of Telecommunications Technology Association.

Netbooks® is a registered trademark of Netbooks, Inc.

Ordering Information

Part Number	Output Voltage ⁽¹⁾	Package	Eco Status	Temperature Range	Packing
FAN5361UC123X	1.233V	WLCSP-6 0.4mm Pitch	Green	–40 to +85°C	Tape and Reel
FAN5361UC182X	1.820V	WEGGE-0 0.4mm Fillin	Green	-40 to +65 C	rape and Reel

Other voltage options available on request. Contact a Fairchild representative.

Pin Configurations



Figure 2. WLCSP, Bumps Facing Down

Figure 3. WLCSP, Bumps Facing Up

Pin Definitions

Pin#	Name	Description			
A1	MODE	MODE . Logic 1 on this pin forces the IC to stay in PWM mode. A logic 0 allows the IC to automatically switch to PFM during light loads. The regulator also synchronizes its switching frequency to four times the frequency provided on this pin. Do not leave this pin floating.			
B1	SW	vitching Node. Connect to output inductor.			
C1	FB	eedback / Vout. Connect to output voltage.			
C2	GND	Ground. Power and IC ground. All signals are referenced to this pin.			
B2	EN	Enable . The device is in shutdown mode when voltage to this pin is <0.4V and enabled when >1.2 Do not leave this pin floating.			
A2	VIN	nput Voltage. Connect to input power source.			

For Fairchild's definition of "green" Eco Status, please visit: http://www.fairchildsemi.com/company/green/rohs_green.html.

Absolute Maximum Ratings

Stresses exceeding the absolute maximum ratings may damage the device. The device may not function or be operable above the recommended operating conditions and stressing the parts to these levels is not recommended. In addition, extended exposure to stresses above the recommended operating conditions may affect device reliability. The absolute maximum ratings are stress ratings only.

Symbol	Parameter		Min.	Max.	Units
V _{IN}	Input Voltage	-0.3	7.0	V	
V _{SW}	Voltage on SW Pin			$V_{IN} + 0.3^{(2)}$	V
V _{CTRL}	EN and MODE Pin Voltage			$V_{IN} + 0.3^{(2)}$	V
	Other Pins		-0.3	$V_{IN} + 0.3^{(2)}$	V
ESD	Electrostatic Discharge	Human Body Model per JESD22-A114	4.0		kV
ESD	Protection Level	Charged Device Model per JESD22-C101	1.5		ΝV
TJ	Junction Temperature		-4 0	+150	°C
T _{STG}	Storage Temperature		-65	+150	°C
TL	Lead Soldering Temperature,	10 Seconds		+260	°C

Note:

2. Lesser of 7V or V_{IN}+0.3V.

Recommended Operating Conditions

The Recommended Operating Conditions table defines the conditions for actual device operation. Recommended operating conditions are specified to ensure optimal performance to the datasheet specifications. Fairchild does not recommend exceeding them or designing to Absolute Maximum Ratings.

Symbol	Parameter	Min.	Тур.	Max.	Units
Vcc	Supply Voltage Range	2.3		5.5	V
I _{OUT}	Output Current	0		600	mA
L	Inductor		0.47		μH
C _{IN}	Input Capacitor		2.2		μF
C _{OUT}	Output Capacitor	1.6	4.7	12.0	μF
T _A	Operating Ambient Temperature	-40	/	+85	°C
TJ	Operating Junction Temperature	-40		+125	°C

Thermal Properties

Junction-to-ambient thermal resistance is a function of application and board layout. This data is measured with four-layer 1s2p boards in accordance to JEDEC standard JESD51. Special attention must be paid not to exceed junction temperature $T_{J(max)}$ at a given ambient temperate T_A .

Symbol	Parameter			Units
θ_{JA}	Junction-to-Ambient Thermal Resistance	WLCSP	150	°C/W

Electrical Characteristics

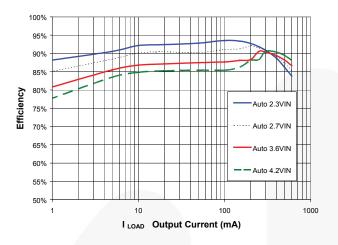
Minimum and maximum values are at V_{IN} = V_{EN} = 2.3V to 5.5V, V_{MODE} = 0V (AUTO Mode), T_A = -40°C to +85°C; circuit of Figure 1, unless otherwise noted. Typical values are at T_A = 25°C, V_{IN} = V_{EN} = 3.6V.

Symbol	Parameter		Conditions	Min.	Тур.	Max.	Units
Power Sup	pplies						
	Quiescent Current Shutdown Supply Current		No load, Not Switching		35	55	μA
ΙQ			PWM Mode		6		mA
I _(SD)			V _{IN} = 3.6V, EN = GND		0.05	1.00	μA
V_{UVLO}			Rising V _{IN}		2.15	2.25	V
V _{UVHYST}	Under-Voltage Locko	out Hysteresis			150		mV
V _(ENH)	Enable HIGH-Level I	nput Voltage		1.2			V
V _(ENL)	Enable LOW-Level In	nput Voltage				0.4	V
I _(EN)	Enable Input Leakag	e Current	EN to V _{IN} or GND		0.01	1.00	μΑ
$V_{(MH)}$	MODE HIGH-Level I	nput Voltage		1.2			V
$V_{(ML)}$	MODE LOW-Level Ir	nput Voltage				0.4	V
I _(M)	MODE Input Leakage	e Current	MODE to V _{IN} or GND		0.01	1.00	μA
Switching	and Synchronization						•
f _{SW}	Switching Frequency	,(3)	V _{IN} = 3.6V, T _A = 25°C	5.4	6.0	6.6	MHz
f _{SYNC}	MODE Synchronizat	ion Range ⁽³⁾	Square Wave at MODE Input	1.3	1.5	1.7	MHz
Regulation	n			\ \			
	Output Voltage	1.82V	$I_{LOAD} = 0$ to $600mA$	1.784	1.820	1.875	V
Vo		1.02 V	PWM Mode	1.784	1.820	1.856	V
VO	Accuracy	1.233V	$I_{LOAD} = 0$ to $600mA$	1.207	1.233	1.272	V
		1.233 V	PWM Mode	1.207	1.233	1.259	V
t _{ss}	Soft-Start		From EN Rising Edge		180	300	μs
Output Dri	iver						
В	PMOS On Resistance		$V_{IN} = V_{GS} = 3.6V$		350		mΩ
$R_{DS(on)}$	NMOS On Resistano	e	$V_{IN} = V_{GS} = 3.6V$		225		mΩ
I _{LIM(OL)}	PMOS Peak Current	Limit	Open-Loop	900	1100	1250	mA
T _{TSD}	Thermal Shutdown		CCM Only		150		°C
T _{HYS}	Thermal Shutdown F	lysteresis			15		°C

Notes:

- 3. Limited by the effect of t_{OFF} minimum (see Figure 13 and Figure 14 in Typical Performance Characteristics).
- 4. The Electrical Characteristics table reflects open-loop data. Refer to Operation Description and Typical Characteristics for closed-loop data.

Typical Performance Characteristics



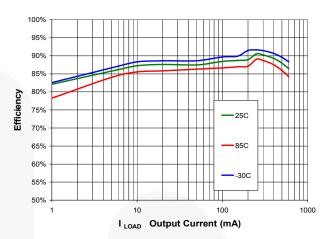
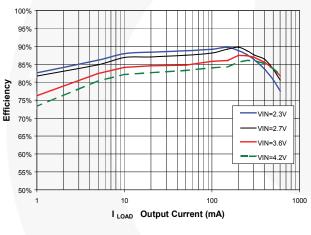


Figure 4. Efficiency vs. Load Current and Input Supply

Figure 5. Efficiency vs. Load Current and Temperature



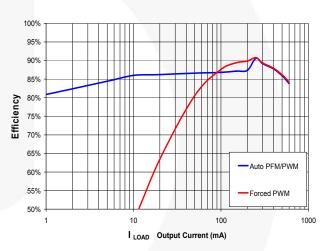
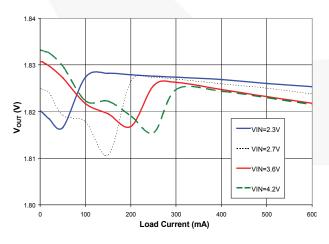


Figure 6. 1.233V_{OUT} Efficiency vs. Load Current and Supply Figure 7. Efficiency, Auto PWM/PFM vs. Forced PWM



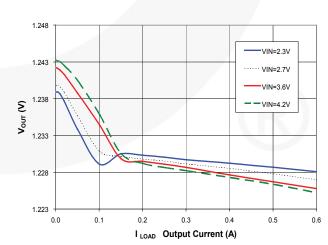
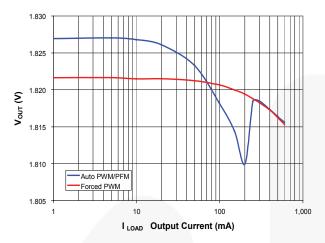


Figure 8. Load Regulation

Figure 9. 1.233V_{OUT} Load Regulation vs. Input Supply



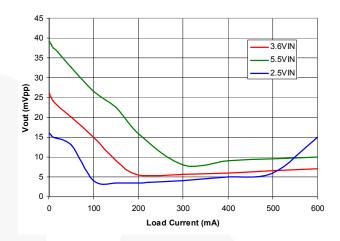
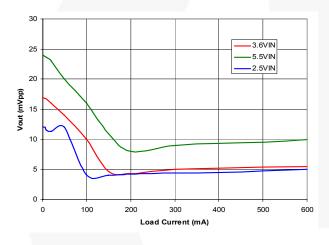


Figure 10. Load Regulation, Auto PFM / PWM and Forced PWM

Figure 11. 1.82V_{OUT} Peak-to-Peak Output Voltage Ripple



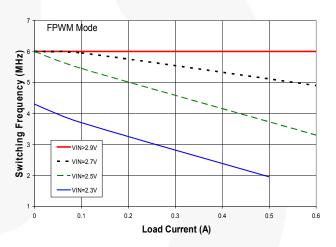
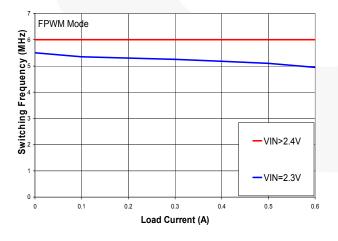


Figure 12. 1.233V_{OUT} Peak-to-Peak Output Voltage Ripple

Figure 13. Effect of t_{OFF(MIN)} on reducing the Switching Frequency



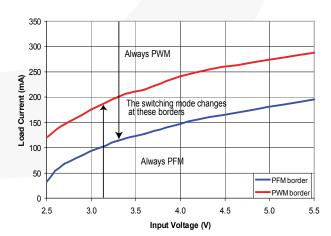
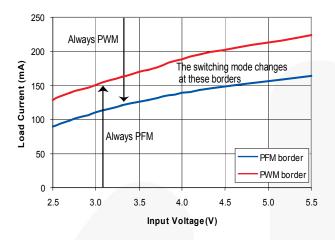


Figure 14. 1.233V_{OUT} Effect of t_{OFF(MIN)} on reducing the Switching Frequency

Figure 15. PFM / PWM Boundaries



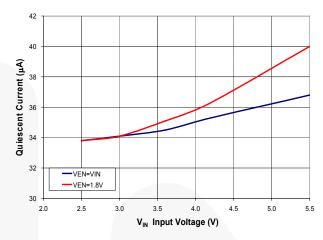


Figure 16. 1.233V_{OUT} PFM / PWM Boundaries

Figure 17. Quiescent Current vs. Input Voltage

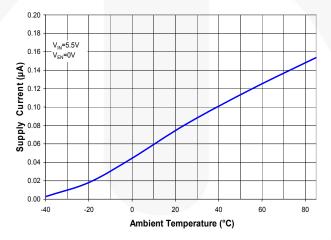


Figure 18. Shutdown Current vs. Temperature

Unless otherwise noted, V_{IN} = V_{EN} = 3.6V, V_{MODE} = 0V (AUTO Mode), V_{OUT} = 1.82V, T_A = 25°C, 5µs/div. horizontal sweep.

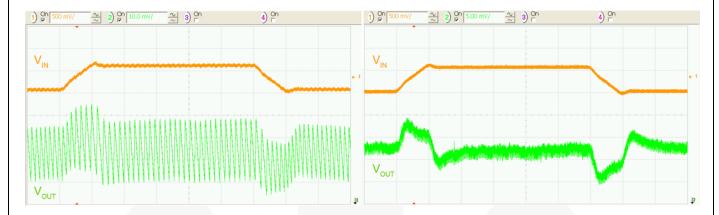


Figure 19. Line Transient 3.3V_{IN} to 3.9V_{IN}, 50mA Load, 10µs/div.

Figure 20. Line Transient 3.3V_{IN} to 3.9V_{IN}, 250mA Load, 10µs/div.

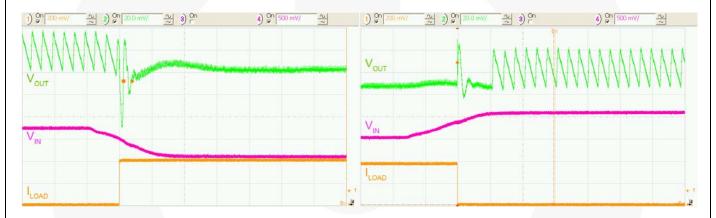


Figure 21. Combined Line/Load Transient 3.9 to 3.3V_{IN} Combined with 40mA to 400mA Load Transient

Figure 22. Combined Line/Load Transient 3.3 to 3.9V_{IN} Combined with 400mA to 40mA Load Transient

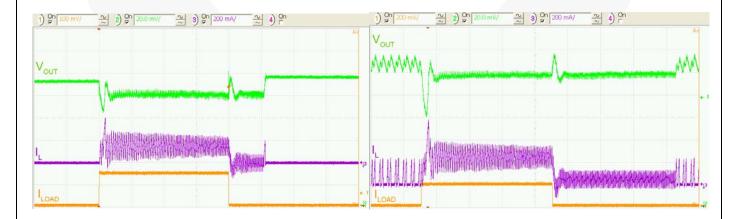
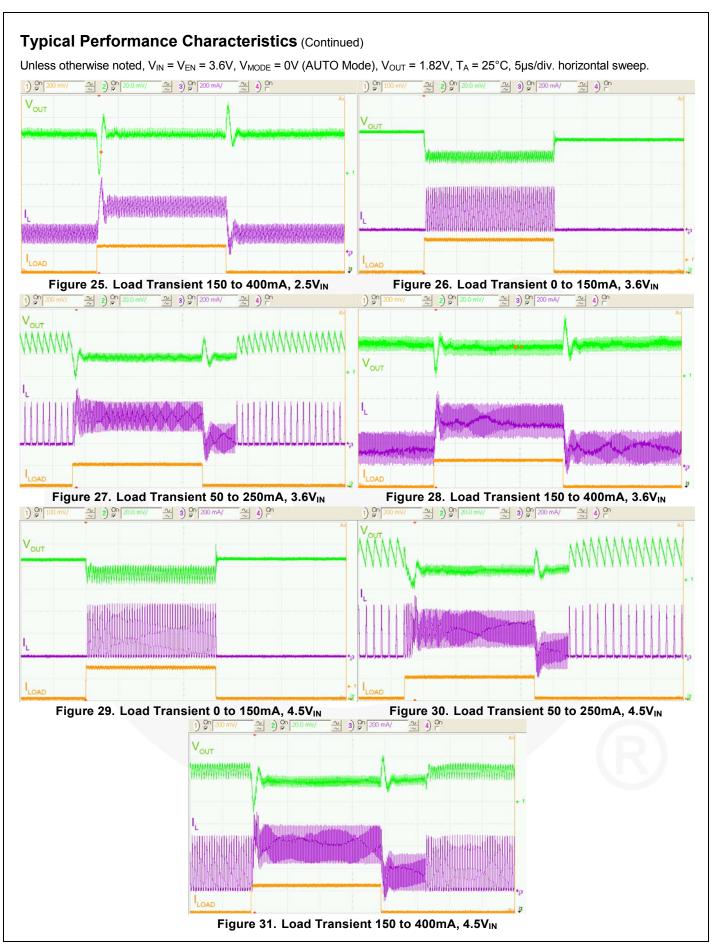


Figure 23. Load Transient 0 to 150mA, 2.5V_{IN}

Figure 24. Load Transient 50 to 250mA, 2.5V_{IN}



Unless otherwise noted, $V_{IN} = V_{EN} = 3.6V$, $V_{MODE} = 0V$ (AUTO Mode), $V_{OUT} = 1.82V$, $T_A = 25$ °C, $5\mu s/div$. horizontal sweep.

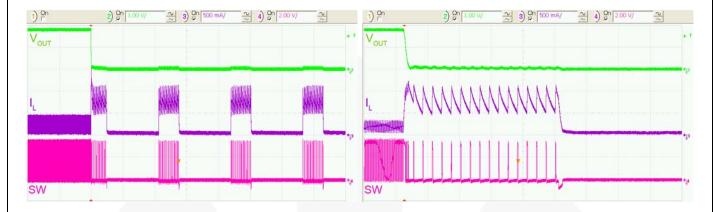


Figure 32. Metallic Short Applied at V_{OUT} , $50\mu\text{s}/\text{div}$.

Figure 33. Metallic Short Applied at V_{OUT}

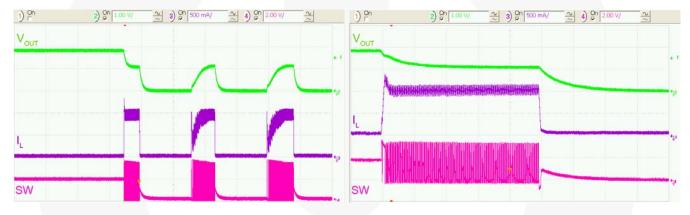


Figure 34. Over-Current Fault Response, $R_{LOAD} = 1\Omega$, 50μ s/div.

Figure 35. Over-Current Fault Response, R_{LOAD} = 1Ω



Figure 36. Overload Recovery to Light Load, 50µs/div.

Figure 37. Soft-Start, R_{LOAD} = 50 Ω , 20 μ s/div.



Figure 38. SW-Node Jitter (Infinite Persistence), I_{LOAD} = 200mA, 50ns/div.

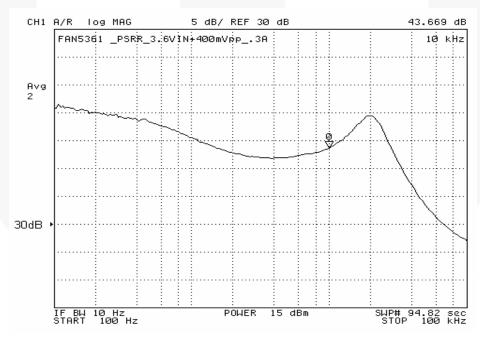


Figure 39. Power Supply Rejection Ratio at 300mA Load

Operation Description

The FAN5361 is a 600mA, step-down, switching voltage regulator that delivers a fixed output from an input voltage supply of 2.3V to 5.5V. Using a proprietary architecture with synchronous rectification, the FAN5361 is capable of delivering a peak efficiency of 92%, while maintaining efficiency over 80% at load currents as low as 1mA. The regulator operates at a nominal frequency of 6MHz at full load, which reduces the value of the external components to 470nH for the inductor and $4.7\mu F$ for the output capacitor.

Control Scheme

The FAN5361 uses a proprietary, non-linear, fixed-frequency PWM modulator to deliver a fast load transient response, while maintaining a constant switching frequency over a wide range of operating conditions. The regulator performance is independent of the output capacitor ESR, allowing for the use of ceramic output capacitors. Although this type of operation normally results in a switching frequency that varies with input voltage and load current, an internal frequency loop holds the switching frequency constant over a large range of input voltages and load currents.

For very light loads, the FAN5361 operates in discontinuous current (DCM) single-pulse PFM mode, which produces low output ripple compared with other PFM architectures. Transition between PWM and PFM is seamless, with a glitch of less than 18mV at V_{OUT} during the transition between DCM and CCM modes.

Combined with exceptional transient response characteristics, the very low quiescent current of the controller (35 μ A) maintains high efficiency; even at very light loads, while preserving fast transient response for applications requiring tight output regulation.

Enable and Soft-Start

When EN is LOW, all circuits in FAN5361 are off and the IC draws ~50nA of current. When EN is HIGH and V_{IN} is above its UVLO threshold, the regulator begins a soft-start cycle. The output ramp during soft-start is a fixed slew rate of 50mV/ μ s from 0 to 1 V_{OUT} , then 12.5mV/ μ s until the output reaches its setpoint. Regardless of the state of the MODE pin, PFM mode is enabled to prevent current from being discharged from C_{OUT} if soft-start begins when C_{OUT} is charged.

The IC may fail to start if heavy load is applied during startup and/or if excessive C_{OUT} is used. This is due to the current-limit fault response, which protects the IC in the event of an over-current condition present during soft-start.

The current required to charge C_{OUT} during soft-start is commonly referred to as "displacement current" is given as:

$$I_{DISP} = C_{OUT} \bullet \frac{dV}{dt}$$
 (1)

where the $\frac{\mbox{d} \mbox{V}}{\mbox{d} \mbox{t}}$ term refers to the soft-start slew rate above.

To prevent shut-down during soft-start, the following condition must be met:

$$I_{DISP} + I_{LOAD} < I_{MAX(DC)}$$
 (2)

where $I_{MAX(DC)}$ is the maximum load current the IC is guaranteed to support (600mA).

Table 1 shows combinations of C_{OUT} that allow the IC to start successfully with the minimum R_{LOAD} that can be supported.

Table 1. Minimum R_{LOAD} Values for Soft-Start with Various C_{OUT} Values

C _{OUT}	Minimum R _{LOAD}
4.7μF, 0402	V _{OUT} / 0.60
2 X 4.7μF, 0402	V _{OUT} / 0.60
10μF, 0603	V _{OUT} / 0.60
10μF, 0805	V _{OUT} / 0.50

Startup into Large Cout

Multiple soft-start cycles are required for no-load startup if C_{OUT} is greater than 15 μ F. Large C_{OUT} requires light initial load to ensure the FAN5361 starts appropriately. The IC shuts down for 85 μ s when IDISP exceeds ILIMIT for more than 21 μ s of current limit. The IC then begins a new soft-start cycle. Since C_{OUT} retains its charge when the IC is off, the IC reaches regulation after multiple soft-start attempts.

MODE Pin

Logic 1 on this pin forces the IC to stay in PWM mode. A logic 0 allows the IC to automatically switch to PFM during light loads. If the MODE pin is toggled, the converter synchronizes its switching frequency to four times the frequency on the mode pin (f_{MODE}).

At startup, the mode pin must be held LOW for at least $10\mu s$ or HIGH for $10\mu s$ to ensure that the converter does not attempt to synchronize to this pin.

Current Limit, Fault Shutdown, and Restart

A heavy load or short circuit on the output causes the current in the inductor to increase until a maximum current threshold is reached in the high-side switch. Upon reaching this point, the high-side switch turns off, preventing high currents from causing damage. The regulator continues to limit the current cycle-by-cycle. After 21 μ s of current limit, the regulator triggers an over-current fault, causing the regulator to shut down for about 85 μ s before attempting a restart.

If the fault was caused by short circuit, the soft-start circuit attempts to restart and produces an over-current fault after about $32\mu s$, which results in a duty cycle of less than 30%, limiting power dissipation.

The closed-loop peak-current limit, $I_{LIM(PK)}$, is not the same as the open-loop tested current limit, $I_{LIM(OL)}$, in the Electrical Characteristics table. This is primarily due to the effect of propagation delays of the IC current limit comparator.

Under-Voltage Lockout (UVLO)

When EN is HIGH, the under-voltage lockout keeps the part from operating until the input supply voltage rises high enough to properly operate. This ensures no misbehavior of the regulator during startup or shutdown.

Thermal Shutdown (TSD)

When the die temperature increases, due to a high load condition and/or a high ambient temperature, the output switching is disabled until the temperature on the die has fallen sufficiently. The junction temperature at which the thermal shutdown activates is nominally 150°C with a 15°C hysteresis.

Minimum Off-Time Effect on Switching Frequency

 ${
m to_{FF(MIN)}}$ is 50ns. This imposes constraints on the maximum ${V_{OUT}\over V_{IN}}$ that the FAN5361 can provide, or the maximum

output voltage it can provide at low V_{OUT} while maintaining a fixed switching frequency in PWM mode.

When V_{IN} is high, fixed switching is maintained as long as V_{IN}

$$\frac{V_{OUT}}{V_{IN}} \le 1 - t_{OFF(MIN)} \bullet f_{SW} \approx 0.7 .$$

The switching frequency drops when the regulator cannot provide sufficient duty cycle at 6MHz to maintain regulation. This occurs when V_{OUT} is 1.82V and V_{IN} is below 2.9V at high load currents (see Figure 14).

The calculation for switching frequency is given by:

$$f_{SW} = \min\left(\frac{1}{t_{SW(MAX)}}, 6MHz\right)$$
 (3)

where:

$$t_{SW(MAX)} = 50 \, ns \, \bullet \left(1 + \frac{V_{OUT} + I_{OUT} \bullet R_{OFF}}{V_{IN} - I_{OUT} \bullet R_{ON} - V_{OUT}} \right) \tag{4}$$

where:

$$R_{OFF} = R_{DSON_N} + DCR_L$$

$$R_{ON} = R_{DSON} P + DCR_L$$

Applications Information

Selecting the Inductor

The output inductor must meet both the required inductance and the energy handling capability of the application. The inductor value affects average current limit, the PWM-to-PFM transition point, output voltage ripple, and efficiency.

The ripple current (ΔI) of the regulator is:

$$\Delta I \approx \frac{V_{OUT}}{V_{IN}} \bullet \left(\frac{V_{IN} - V_{OUT}}{L \bullet f_{SW}} \right)$$
 (5)

The maximum average load current, $I_{MAX(LOAD)}$, is related to the peak current limit, $I_{LIM(PK)}$ by the ripple current, given by:

$$I_{MAX(LOAD)} = I_{LIM(PK)} - \frac{\Delta I}{2}$$
 (6)

The transition between PFM and PWM operation is determined by the point at which the inductor valley current crosses zero. The regulator DC current when the inductor current crosses zero, I_{DCM}, is:

$$I_{DCM} = \frac{\Delta I}{2} \tag{7}$$

The FAN5361 is optimized for operation with L = 470nH, but is stable with inductances up to 1.2 μ H (nominal). The inductor should be rated to maintain at least 80% of its value at $I_{\text{LIM}(PK)}$.

Efficiency is affected by the inductor DCR and inductance value. Decreasing the inductor value for a given physical size typically decreases the DCR; but since ΔI increases, the RMS current increases, as do the core and skin effect losses.

$$I_{RMS} = \sqrt{I_{OUT(DC)}^2 + \frac{\Delta I^2}{12}}$$
 (8)

The increased RMS current produces higher losses through the R_{DS(ON)} of the IC MOSFETs, as well as the inductor DCR.

Increasing the inductor value produces lower RMS currents, but degrades transient response. For a given physical inductor size, increased inductance usually results in an inductor with lower saturation current and higher DCR.

Table 2 shows the effects of inductance higher or lower than the recommended 470nH on regulator performance.

Output Capacitor

Table 3 suggests 0402 capacitors. 0603 capacitors may further improve performance in that the effective capacitance is higher. This improves transient response and output ripple.

Increasing C_{OUT} has no effect on loop stability and can therefore be increased to reduce output voltage ripple or to improve transient response. Output voltage ripple, ΔV_{OUT} , is:

$$\Delta V_{OUT} = \Delta I \bullet \left(\frac{1}{8 \bullet C_{OUT} \bullet f_{SW}} + ESR \right)$$
 (9)

Input Capacitor

The $2.2\mu F$ ceramic input capacitor should be placed as close as possible between the VIN pin and GND to minimize the parasitic inductance. If a long wire is used to bring power to the IC, additional "bulk" capacitance (electrolytic or tantalum) should be placed between C_{IN} and the power source lead to reduce ringing that can occur between the inductance of the power source leads and C_{IN} .

The effective capacitance value decreases as V_{IN} increases due to DC bias effects.

Table 2. Effects of Changes in Inductor Value (from 470nH Recommended Value) on Regulator Performance

Inductor Value I _{MAX(LOAD)}		$\Delta extsf{V}_{OUT}$	Transient Response
Increase	Increase	Decrease	Degraded
Decrease	Decrease	Increase	Improved

Table 3. Recommended Passive Components and their Variation Due to DC Bias

Component	onent Description Vendor		Min.	Тур.	Max.	Comment
L1	470nH, 2012, 90mΩ,1.1A	Murata LQM21PNR47MC0 Murata LQM21PNR54MG0 Hitachi Metals HSLI-201210AG-R47	300nH	470nH	520nH	Minimum value occurs at maximum current
C _{IN}	2.2μF, 6.3V, X5R, 0402	Murata or Equivalent GRM155R60J225ME15 GRM188R60J225KE19D	1.0μF	2.2μF	2.4μF	Decrease primarily due to DC bias (V _{IN}) and elevated temperature
C _{OUT} 4.7μF, X5R, 0402		Murata or Equivalent GRM155R60G475M GRM155R60E475ME760	1.6μF	4.7μF	5.2μF	Decrease primarily due to DC bias (V _{OUT})

PCB Layout Guidelines

There are only three external components: the inductor and the input and output capacitors. For any buck switcher IC, including the FAN5361, it is important to place a low-ESR input capacitor very close to the IC, as shown in Figure 40. The input capacitor ensures good input decoupling, which helps reduce noise appearing at the output terminals and ensures that the control sections of the IC do not behave

erratically due to excessive noise. This reduces switching cycle jitter and ensures good overall performance. It is important to place the common GND of C_{IN} and C_{OUT} as close as possible to the FAN5361 C2 terminal. There is some flexibility in moving the inductor further away from the IC; in that case, V_{OUT} should be considered at the C_{OUT} terminal.

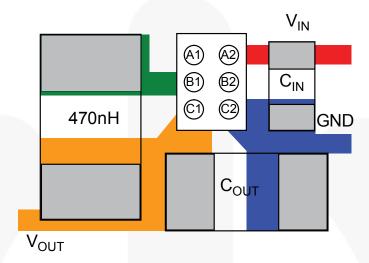
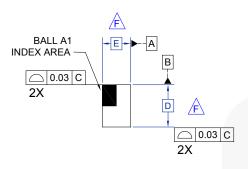
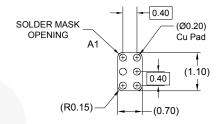


Figure 40. PCB Layout Guidance

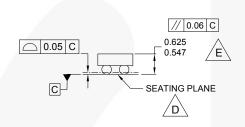
Physical Dimensions

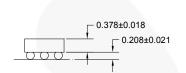




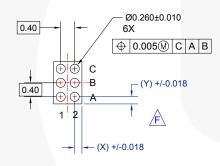
TOP VIEW

RECOMMENDED LAND PATTERN (NSMD)





SIDE VIEWS



BOTTOM VIEW

NOTES:

- A. NO JEDEC REGISTRATION APPLIES.
- B. DIMENSIONS ARE IN MILLIMETERS.
- C. DIMENSIONS AND TOLERANCES PER ASMEY14.5M, 1994.
- D. DATUM C, THE SEATING PLANE IS DEFINED BY THE SPHERICAL CROWNS OF THE BALLS.
- E. PACKAGE TYPICAL HEIGHT IS 586 MICRONS ±39 MICRONS (547-625 MICRONS).
- F. FOR DIMENSIONS D, E, X, AND Y SEE PRODUCT DATASHEET.
 - G. BALL COMPOSITION: Sn95.5-Ag3.9-Cu0.6.
 - H. DRAWING FILENAME: UC006ACrev2.

Figure 41. 6-Bump WLCSP, 0.4mm Pitch

Product Specific Dimensions

Product	D	E	Х	Υ
FAN5361UCX	1.390 +/-0.030	0.990 +/-0.030	0.295	0.295

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